

**Solid state broadband un-cooled
noise generator with noise
temperature below room
temperature**

by

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Overview

- Introduction
- Noise figure measurement uncertainty
- Schottky diode based noise generator
 - I/U characteristics
 - Noise model
- Implementation
- Application and measurements
- Conclusions

Introduction

- For absolute noise figure measurement a lot of problems/errors arise if e.g.
NF < 1dB (= $T_e < 75\text{K}$) – even with sophisticated measurement equipment
- What are reasons/interdependencies for uncertainties?
- Could we lower the uncertainties for NF values below 1dB?

Noise figure measurement uncertainty

- Here only two contributions considered:

1. ENR calibration uncertainty:

2. Instrumentation error:

ALLTech 7615

enr = 15.5dB

$\Delta\text{enr} = \pm 0.3\text{dB}$



HP 8970A/B

$\Delta y = \pm 0.1\text{dB}$

Agilent/HP 346A

enr = 5.2dB

$\Delta\text{enr} = \pm 0.2\text{dB}$



Agilent N8973A

$\Delta y = \pm 0.05\text{dB}$

Agilent N4000A

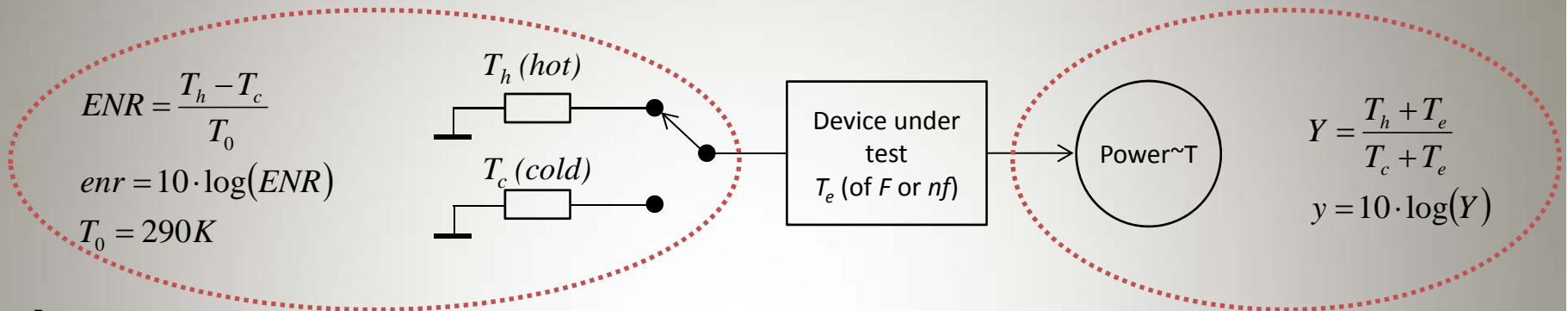
enr = 6dB

$\Delta\text{enr} = \pm 0.15\text{dB}$



Noise figure measurement basics

- Y factor method



→ Noise factor:

$$F = \frac{ENR - Y \cdot (T_c/T_0 - 1)}{Y - 1}$$

or noise figure:

$$nf = 10 \cdot \log(F)$$

- nf uncertainty (see conference paper)

→ Combination of two uncertainties at actual set of parameters:

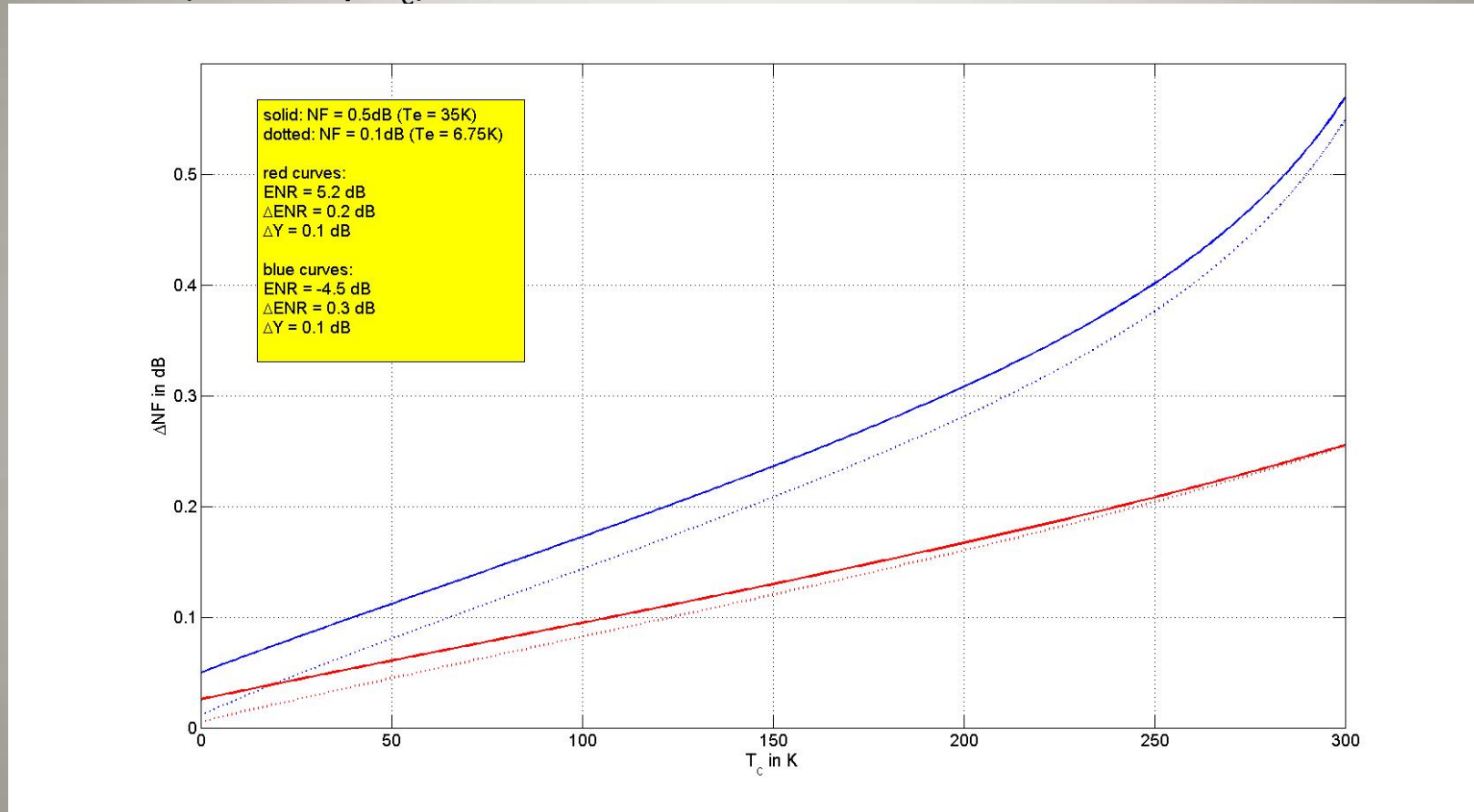
$$\Delta F = \sqrt{\left(\frac{\delta F}{\delta Y} \cdot \Delta Y\right)^2 + \left(\frac{\delta F}{\delta ENR} \cdot \Delta ENR\right)^2}$$

→ nf uncertainty in dB's:

$$\Delta nf = \frac{10}{\log(10)} \cdot \frac{\Delta F}{F}$$

Noise figure measurement uncertainty

- $\Delta nf = f(\Delta enr, \Delta y, T_c)$ for DUT $nf = 0.5\text{dB}$ and $nf = 0.1\text{dB}$



- enr could be much lower than 5dB to measure $nf < 0.5\text{dB}$
- uncertainty dependent on absolute nf value
- make T_c as low as possible!

How to lower T_c (and providing a matched load at the same time)?

- Cooled 50Ω resistor (liquid nitrogen $\rightarrow T_c = \sim 80\text{K}$)
- Looking at cold sky \rightarrow RW3BP's cold horn...



Pro:

+ very low cold temperature $T_c = \sim 15\text{K}$

Con:

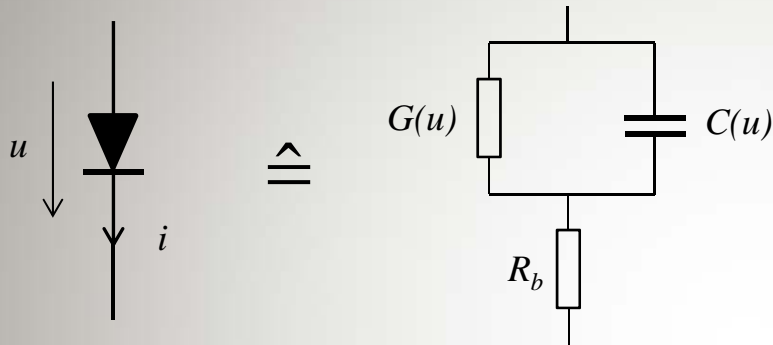
- huge effort

- small band (only 1296MHz or single other band)

- Solid-state Schottky diodes?
 \rightarrow Mixture of shot (Schottky) and thermal (Johnson) noise

Schottky diode based noise generator

- Equivalent circuit of a Schottky diode



$G(u)$: nonlinear conductance of junction
 $C(u)$: nonlinear capacitance of junction
 (very small, e.g. $< 0.5\text{pF} \rightarrow$ high $f!$)
 R_b : bulk resistance (e.g. $< 10\Omega$)

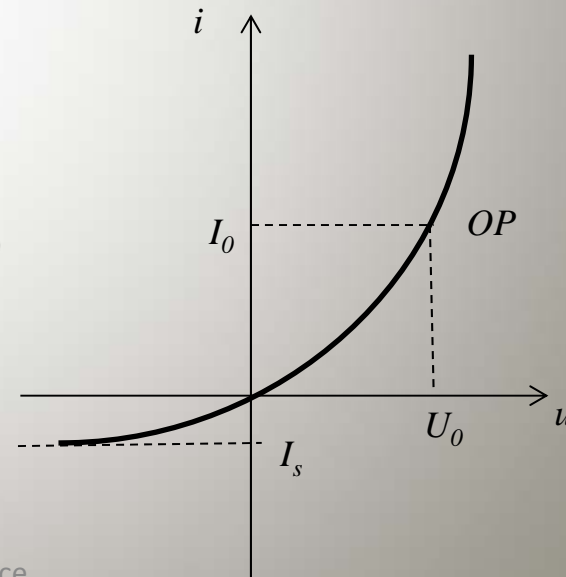
- I/U - characteristics

$$i(u) = I_s \cdot \left(\exp\left(\frac{q \cdot u}{\tilde{n} \cdot kT}\right) - 1 \right)$$

$\frac{kT}{q}$: temperature voltage (26mV at room temp.)

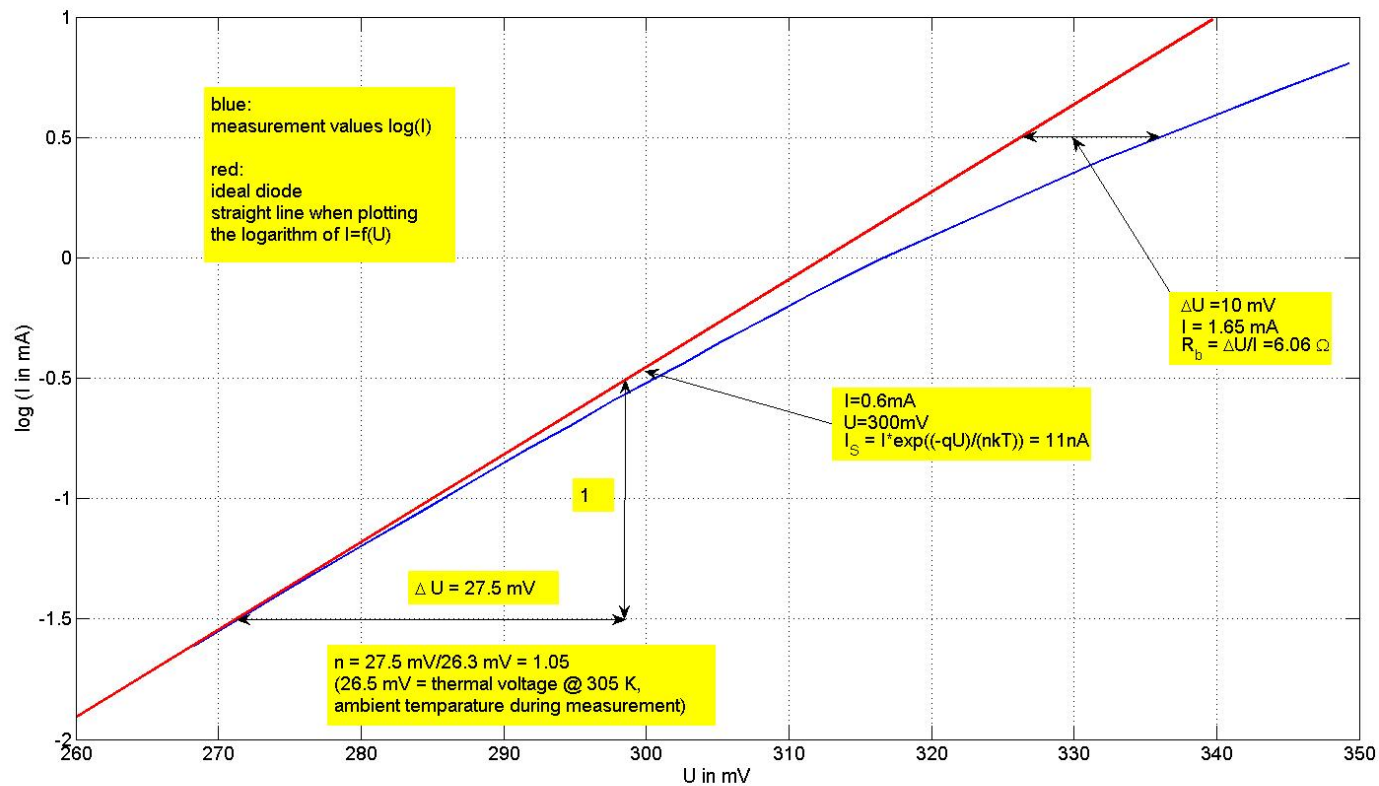
I_s : saturation current (e.g. $< 0.1\mu\text{A}$)

\tilde{n} : ideality factor to describe deviation from exponential, typical values 1...1.2



Schottky diode parameters ?

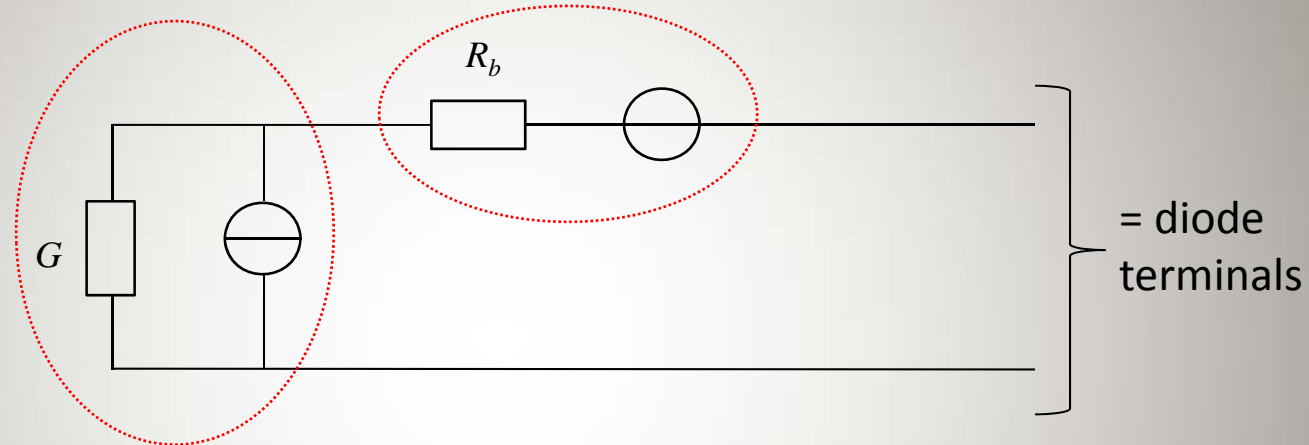
- From data sheet (SPICE parameters)
- Better: measurements, here Agilent HSMS-2823



Schottky diode noise model

thermal (Johnson) noise source:
random motion of charge carriers

shot (Schottky)
noise source:
charge carriers
have to „climb“ a
barrier



Without bulk resistance [1]:

$$\frac{T_{ef}^*}{T} = \frac{1}{2} \cdot \tilde{n} \cdot \left(1 + \frac{I_S}{I_0 + I_S} \right)$$

I_0 : DC current at operating point

T : physical junction temperature
(= ambient room temperature)

Overall noise temperature T_{ef}
including bulk resistance [1]:

$$\frac{T_{ef}}{T} = \frac{\frac{T_{ef}^*}{T} + R_b \cdot G}{1 + R_b \cdot G}$$

[1] Schiek, B.; Rolfes, I.; Siweris, H.-J.:
*Noise in High-Frequency Circuits and
Oscillators*, Wiley, 2006.

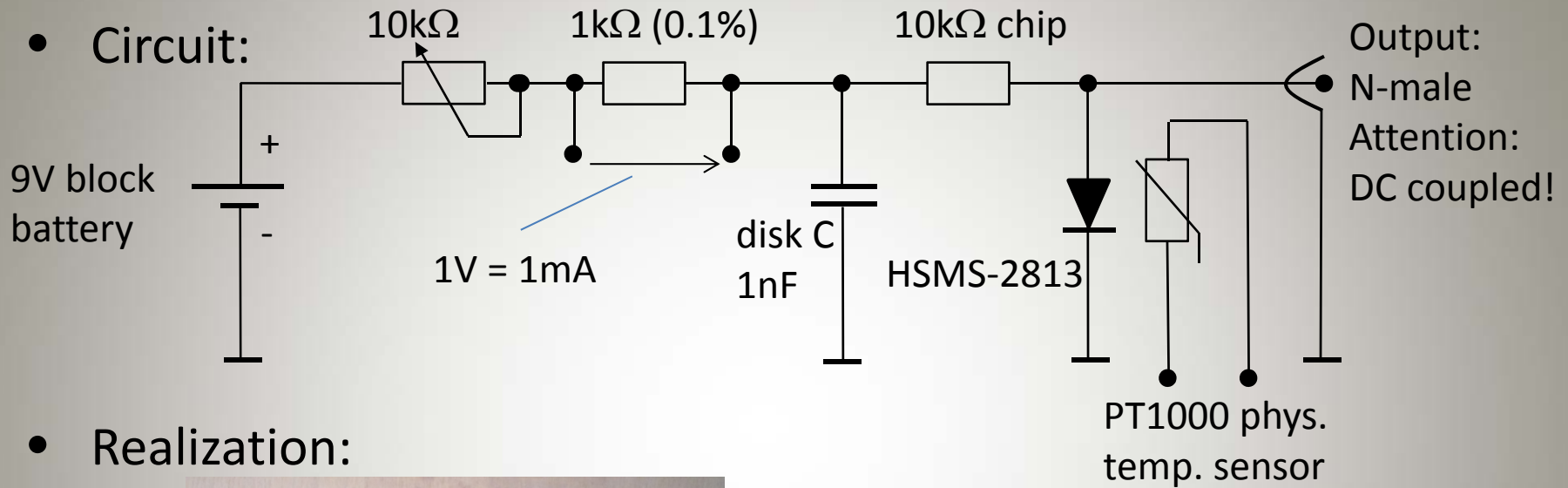
Steps towards Schottky diode noise generator

1. Make I/U measurements (DC measurement) at known ambient temperature to derive
 - Ideality factor
 - Saturation current
 - Bulk resistance
2. Align DC current through diode in order to make bulk resistance in series with differential junction resistance a pure 50Ω load (VNWA measurement) $\rightarrow I/G + R_b = 50\Omega$
3. Apply equation of noise model to calculate effective noise temperature

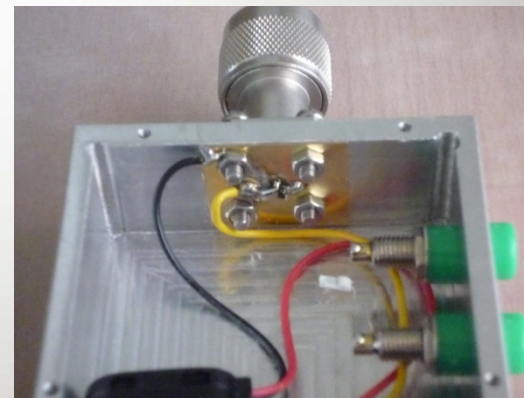


matched cold load with known noise temperature

Implementation



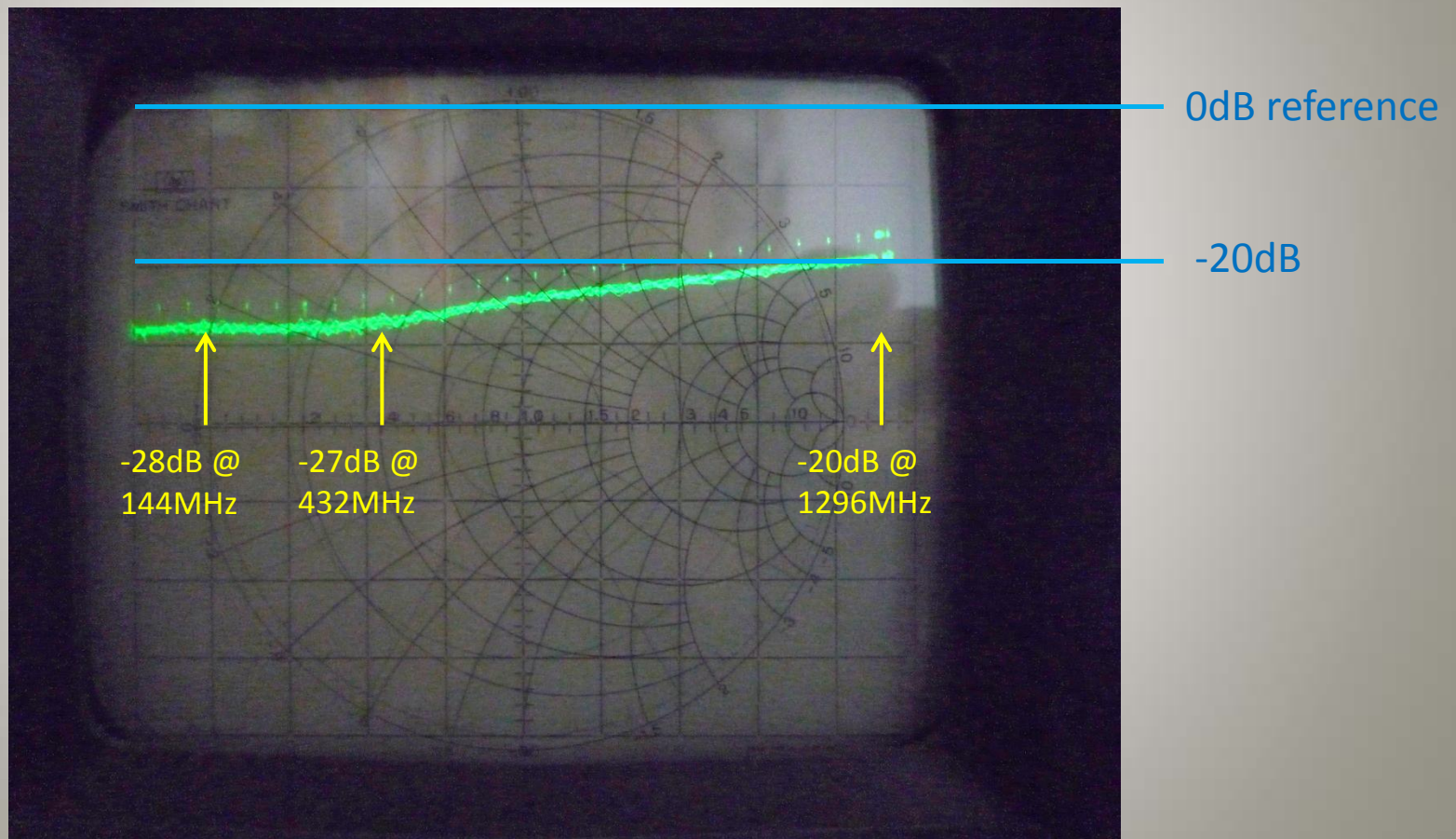
- Realization:



- Effective noise temperature ($I_0=0.67\text{mA}$, $T=305\text{K}$): **180K**

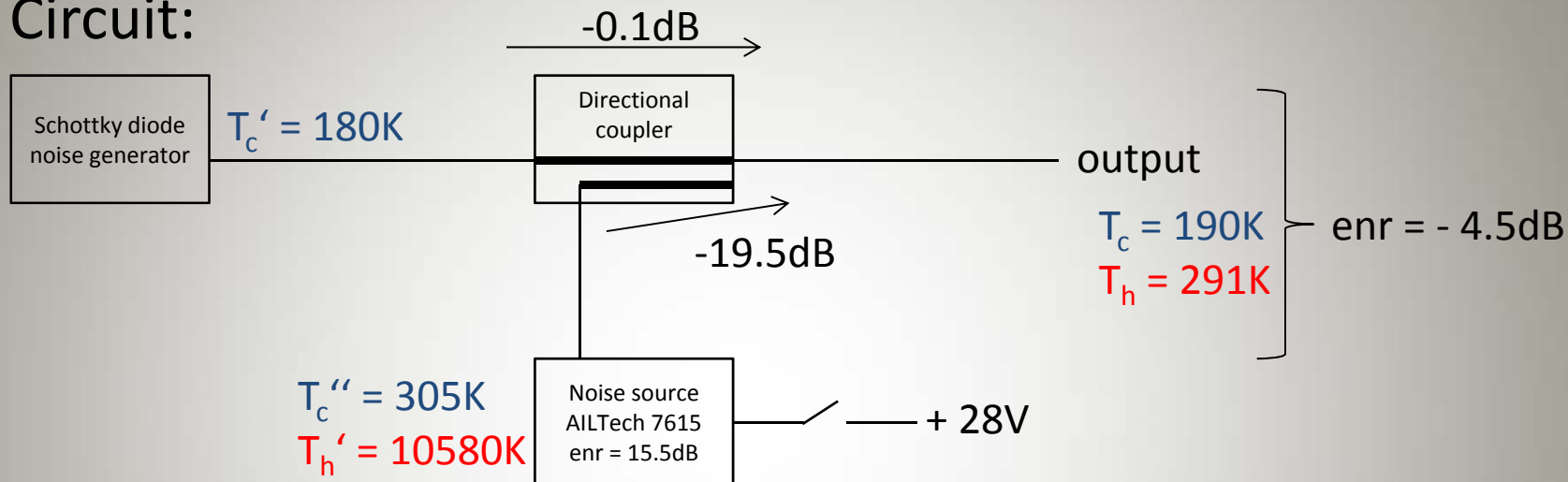
Return loss

- Attention: hold VNWA output low ($< -20\text{dBm}$) during measurement to avoid nonlinear distortion at diode!



Application

- Circuit:

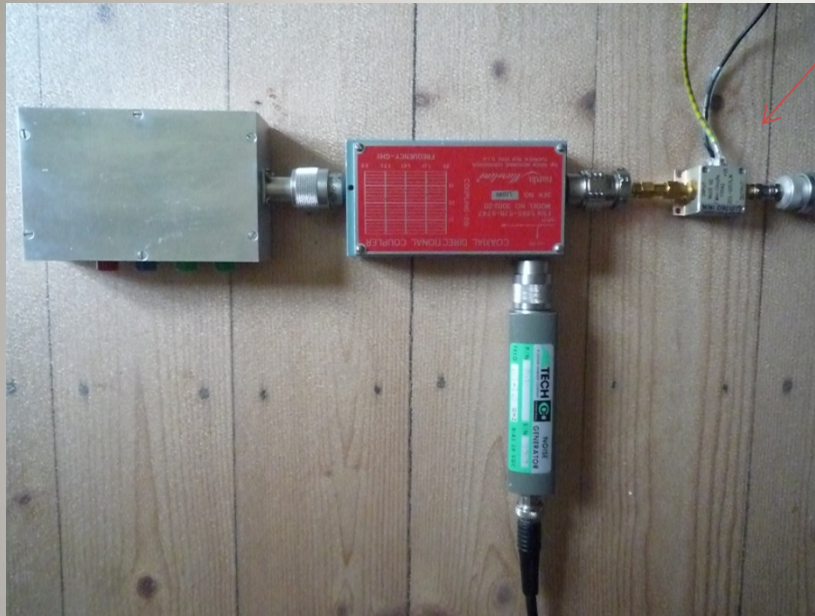


Standard noise source + Schottky diode noise source + coupler
= „new“ noise source:

- $\text{enr} = -4.5\text{dB}$
- $\Delta\text{enr} = 0.3\text{dB}$ (unchanged)
- T_c changed from $\sim 305\text{K}$ to $\sim 190\text{K}$
- Due to -19.5dB coupling factor \rightarrow in fact no gain error due to mismatched LNA (no change in reflection coefficient between „on“ and „off“ state of noise source)

Measurements

- Measurement of MCL ZEL-1217LN @1296MHz



- Results:
 - nf from datasheet: typically 1.1dB
 - measured with HP8970B & HP346A: 0.97dB
 - Measured with Schottky diode noise generator & Narda 1-2 GHz coupler & Alltech 7615: 1dB

Conclusions

- In Y-factor based nf measurements having T_c as low as possible is beneficial
- Matlab based tool to calculate nf uncertainties as function of enr and instrumentation (y-factor) uncertainty
- Schottky diode shows shot and thermal noise
- Realization of simple noise generator with $T_c < T_{amb}$
- Integration of new noise generator into usually used nf measurement setup very easy by means of directional coupler (low loss in main line!)
 - nf uncertainties substantially lowered – not only by low T_c but:
 - Change of reflection coefficient in on/off state of noise source decreased – especially of advantage for amplifiers with mismatched input („gain error“ lowered)
- Application of more expensive diodes for higher frequencies ?